

A Study on the Desulfurization Efficiency of Limestone Sludge with Various Admixtures

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(Received July 1, 2015; Revised October 14, 2015; Accepted October 15, 2015)

ABSTRACT

The flue gas desulfurization (FGD) process is one of the most effective methods to reduce the amount of SO₂ gas (up to 90%) generated by the use of fossil fuel. Limestone is usually used as a desulfurizing agent in the wet-type FGD process; however, the limestone reserves of domestic mines have become exhausted. In this study, limestone sludge produced from the steel works process is used as a desulfurizing agent. Seven different types of additives are also used to improve the efficiency of the desulfurization process. As a result, alkaline additive is identified as the least effective additive, while certain types of organic acids show higher efficiency. It is also observed that the amount of FGD gypsum, which is a by-product of the FGD process, increases with the used of some of those additives.

Key words : FGD systems, Limestone sludge, Organic acid, Alkali admixture agent, Gypsum

1. Introduction

In the early 20th century, the usage of fossil fuels was increased explosively as the industry was developed drastically. Also, with an increase in the usage of fossil fuels, environment contamination problems emerged, and environment regulations for discharge of contaminants were started in the middle of the 20th century in the advanced countries such as US, Germany, Japan as a center. To respond to such environment regulations, studies on processing technology for contaminants were actively conducted, with the interests being concentrated on the processing technologies for NO_x, SO_x, etc. in particular.

Flue Gas desulfurization (FGD) is a removal method for SO₂ gas where the removal ratio of sulfur oxides produced by use of fossil fuels reaches a level of 90%.¹⁾ Flue Gas desulfurization refers to a technique for removing SO_x contained in the exhaust gas after combustion by using the principles of Absorption, Adsorption, Oxidation and Reduction, etc. The existing FGD techniques may be divided into the dry method and the wet method, depending on the water contents of the desulfurizing agent. As a representative desulfurizing agent used for wet FGD technique, magnesium hydroxide (Mg(OH)₂) and limestone may be named, and the limestone of lower prices compared with those of the magnesium hydroxide (Mg(OH)₂) is mainly used domestically. However, since the use of low-quality limestone is almost

impossible for the reasons of operation efficiency and economy, etc., only high-quality limestone is used as the desulfurizing agent. However, as the domestic high-quality limestone is employed as the main and subsidiary raw materials by cement manufacturers, ironworks, etc., a limit of the reserves is being revealed. Consequently, development of desulfurizing agents to substitute for the high-quality limestone is being actively performed, and the study to use limestone sludge produced at ironworks as a desulfurizing agent may be considered as an example.²⁾ The limestone sludge refers to a designated waste of about 15% in moisture content level which is produced upon manufacturing of quicklime used as a subsidiary material in the iron making process, and the desulfurizing effects may be obtained on an equivalent level to that for the existing limestone slurry when removal tests for SO₂ are conducted after mixing of the limestone slurry used in the existing desulfurizing process with the limestone sludge by a given ratio.²⁾

Meanwhile, efficiencies and operation costs of FGD process to remove SO₂ are affected by several factors. Particularly, the removal efficiency of SO₂ gas is determined by pH, temperature, solid content, etc. of the slurry used as a desulfurizing agent for the wet FGD process. Particularly, degradation phenomena for solubility and dissolution rate of SO₂ gas are suppressed when pH of the slurry is low, while degradation in solubility and dissolution rate occurs when the pH is high. To solve this problem, either the amount of limestone is controlled or the buffering admixtures for pH control or the alkali admixtures to improve material transfer rates of SO₂ etc. are employed.^{3,4)}

Therefore, in the present study, the measures allowing improvement of desulfurizing efficiencies of the limestone

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sludge were reviewed by comparative evaluation of desulfurizing performance of each admixture after application of organic acids and alkali admixtures to the limestone sludge.

2. Experimental Procedure

For comparative evaluation of performance of the desulfurizing agent as a function of admixture types, experiments for comparison of desulfurizing efficiencies were conducted. As the desulfurizing agents used for the experiments, samples of the limestone slurry currently used for desulfurizing process at the thermal power plant B mixed with the limestone sludge from the ironwork H by the ratio of 6:4 were used with the moisture content being controlled to be 70%. Also, the admixtures used for performance evaluation included DBA, OR(acidic solution prepared by fermentation of food wastes) and H_2SO_4 , MgO, $MgSO_4$, Acetic acid, Formic acid, etc. The added amounts of the above admixtures compared with the total amount of desulfurizing agents were controlled to be 1%, 3%, 5%, and the pH characteristics, the desulfurizing efficiencies and the produced amount of gypsum, etc. were comparatively evaluated.

As a method for comparative evaluation of desulfurizing efficiencies, gas removal experiment was conducted by using a sealed desiccator, with 500 ppm of SO_2 being prepared (N2 balance) and used as a Flue gas. In the experimental procedure, 17 g of desulfurizing agent was placed in the sealed desiccator, followed by injection of 500 ppm of SO_2 gas for 2 minutes, and the concentrations of SO_2 were measured at each time (0 min, 10 min, 30 min, 60 min, 90 min) by using a direct reading-type gas detector tube (GV-110S, GASTEC Co., JAPAN) after which the desulfurizing efficiencies were measured (Fig. 1). For the desulfurizing agent with the measurement for concentration of SO_2 gas completed, X-ray diffraction (XRD) patterns were measured by using a X-ray diffraction analyzer (D5005D, Siemens Co., GERMANY) after drying for 12 h in a dryer at 40°C (J-300M, JISICO Co., KOREA), and G/C ratios (Gypsum main



Fig. 1. Desulfurization experiment.

peak intensity / Calcite main peak intensity) were calculated for comparative analysis of reaction efficiencies of the desulfurizing agents.

For the samples with the analysis of XRD pattern completed, observation and EDS qualitative analysis of the microstructures of limestone sludge were conducted by using a scanning electron microscope (SM300, TOPCON Co., JAPAN) to perform analyses of shape and purity, etc. for the produced gypsum.

3. Results and Discussion

Types of the admixture may be classified into water-soluble alkali admixtures and organic acid admixtures, and the water-soluble alkali admixtures are in the form of sulfite, sulfate, carbonate, hydroxide salts which improve the material transfer rates of SO_2 by being dissolved in water and providing basicity.⁵⁾ Also, the organic acid has a buffering action in the reactor, with the admixtures for such action should act as an alkali in the solution where the reaction occurs. Such admixtures should have the buffering capability at gas-liquid interfaces (pH 3 ~ 3.5) and in the whole reaction solution (pH 5 ~ 5.5).⁶⁾

The pH characteristics as a function of admixture mixing are shown in Table 1.

When pH changes of the slurry are considered as a function of admixture mixing, the pH is lowered as the contents of acidic admixture are increased, while the pH changes as a function of the alkali admixture content were not shown to be large. Particularly, the pH changes resulting from mixing of DBA and sulfuric acid were shown to be large, which is considered to be caused by the fact that both DBA and sulfuric acid have a strong acidity. After 17 g of the sample with completion of pH measurement was taken, the experiments for measuring the change in SO_2 concentrations were conducted by using a desiccator, with the results shown in Fig. 2.

When the changes in SO_2 gas concentration are considered as a function of types and contents of the admixture, drastic reaction could be seen to have occurred during the initial 30 minutes. Also, in the reaction section during the initial 30 minutes, the removal rates of DBA and SO_2 gas of sulfuric acid were shown to be slower as compared with other admixtures, which is attributed to the pH effect of the desulfurizing agent. In general, the removal rates of SO_2 gas are known to be the higher, the higher the injected L/G ratios and the pH's, and the pH control technique can be seen to be an important factor upon removal reaction of SO_2 gas.

Table 1. pH Characteristics as a Function of Admixture Agent

Mixed amount (wt%)	DBA	OR	Acetic acid	Formic acid	H_2SO_4	MgO	$MgSO_4$
0				7.64			
1	6.17	7.18	6.96	6.90	6.24	7.66	7.63
3	5.49	7.03	6.54	6.48	5.42	7.68	7.67
5	5.34	6.35	6.10	6.01	5.28	7.71	7.70

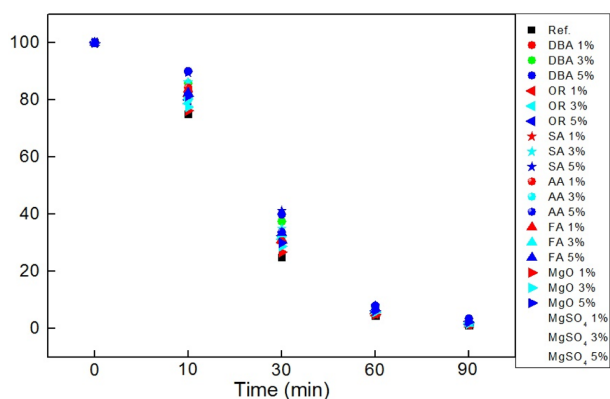


Fig. 2. Changes in SO₂ concentration as a function of admixture (*SA : Sulfuric Acid, AA : Acetic Acid, FA : Formic Acid).

After completing the measurement of SO₂ gas concentrations, and taking the samples showing a satisfactory desulfurizing efficiency for respective drying in a dryer at 40°C for 12 h, XRD patterns were measured, and an example for the analysis results is shown in Fig. 3 and Table 2.

Considering the analysis results for XRD patterns as a function of admixture types, production of gypsum crystals was affirmed to be satisfactory in the samples with addition of 3% of DBA, 3% of OR and 1% of sulfuric acid. This suggests that the admixtures have sufficiently performed the buffering role for controlling pH of the desulfurizing agent in the solution. In addition, when G/C ratios shown in Table 2 were compared, the G/C ratio was affirmed to appear

Table 2. Main Peak Intensity as a Function of Admixture (unit : cps)

	Calcite	Gypsum	G/C ratio
DBA 3%	3424	1083	0.32
OR 3%	3282	1099	0.33
Sulfuric acid 1%	3137	1099	0.35

slightly higher when OR and sulfuric acid were added compared with DBA which was universally employed in the conventional thermal power plants. Based on this, the pH buffering performance of OR can be seen to be higher than the equivalent as compared with that of DBA. Particularly, in the case of sulfuric acid, production of gypsum is considered to have been facilitated upon desulfurizing reaction as SO₃²⁻ ions in the sulfuric acid solution performed not only a pH-buffering role but also a seed role enabling the production of gypsum. However, since OR is a solution prepared by fermentation of food wastes, there exist odors, while use for the process is considered possible in the case of sulfuric acid after the problems of having to pay attention in use, etc. have been solved.

Lastly, after taking the samples with addition of 1% of sulfuric acid for which the XRD pattern analysis had been completed, observation and EDS qualitative analysis of microstructures were conducted for limestone sludge by using a scanning electron microscope to analyze shapes and chemical compositions of the produced gypsum, with the results shown in Fig. 4.

Particle sizes of desulfurized gypsum are reported to be

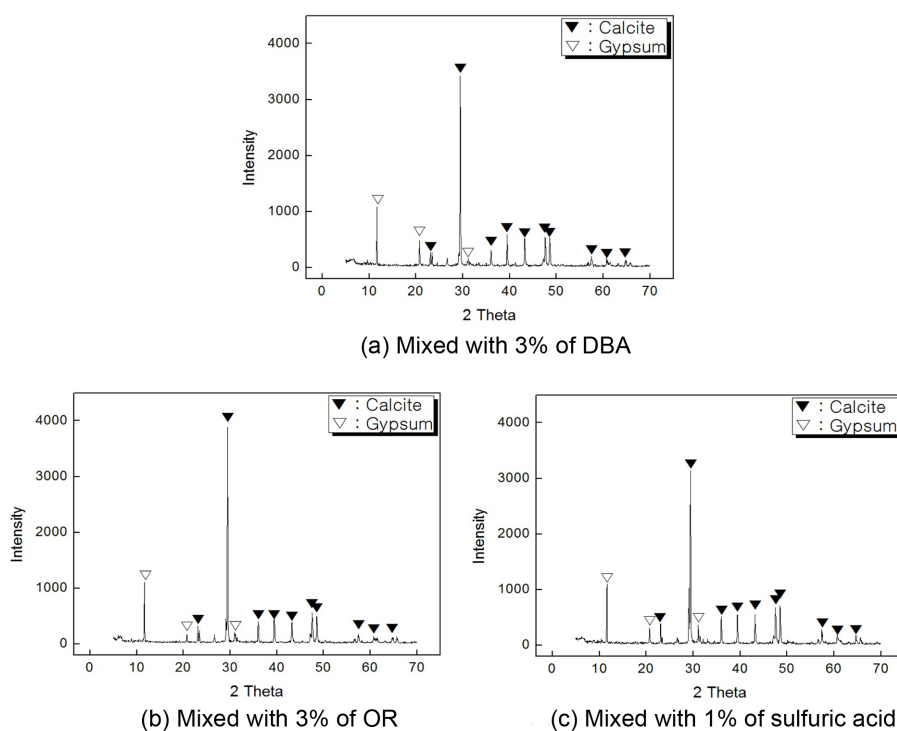


Fig. 3. XRD patterns of admixture.

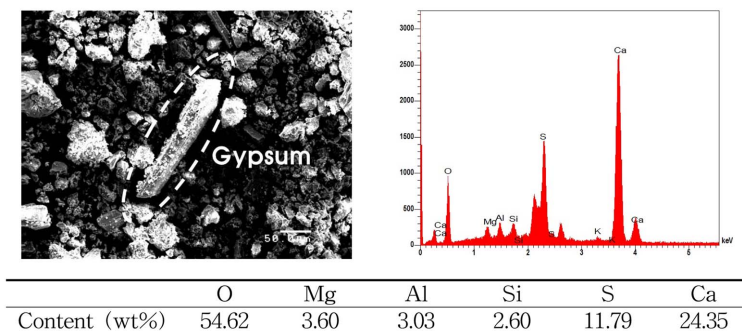


Fig. 4. Microstructure (200x) and EDS analysis of desulfurizing agent with 1% of H_2SO_4 .

affected by the amount of inlet concentration of oxygen, and the crystal shapes affected by the pH and the stirring rate. Also, the crystal shapes show much variation depending on the several impurities contained in the limestone, and the gypsum shapes are known to be transformed from a plate shape to a needle shape as the quality of limestone is degraded.⁷⁾ Considering the picture for observation of a microstructure in Fig. 4, the shape of the produced gypsum is shown to be near a needle shape, although $CaCO_3$ content of the limestone sludge used in the experiment was on the level of about 92%, corresponding to a high-quality limestone. This production of the needle-shaped gypsum is considered attributable to the several impurities contained in the limestone sludge.

4. Conclusions

By using as the desulfurizing agent the samples of mixture of the limestone slurry used by thermal power plants and the limestone sludge produced in iron-making processes, experiments for comparison of desulfurizing performance were conducted as a function of types and contents of the admixture.

According to the experimental results for removal of SO_2 gas, noteworthy results were observed in the increase of desulfurizing efficiencies due to DBA, OR(acidic solution prepared by fermentation of food wastes) and sulfuric acid, although the changes in desulfurizing efficiencies resulting from alkali admixtures were shown to be slight. According to the results of considering Gypsum/Calcite ratios through analysis of desulfurizing efficiencies and XRD patterns, in particular, it could be seen that the most satisfactory desulfurization efficiency was exhibited when OR and sulfuric acid were added. However, there exist odors in the case of OR since it is a solution prepared by fermentation of food wastes, while use in the process is considered possible in the case of sulfuric acid after the problems of having to pay attention in use, etc. have been solved.

Also, according to the observation results for microstructures of the produced desulfurized gypsum by using a scanning electron microscope, needle-shaped desulfurized

gypsum was observed. This suggests that low-quality desulfurized gypsum was produced due to the effects of the impurities contained in limestone sludge even if desulfurizing reaction was implemented by using high-quality limestone. Thus, it is considered that the measures to improve a purity of the produced desulfurized gypsum should be reviewed through continuous research and development in the future.

Based on the above experimental results, it is considered that economic and eco-friendly effects may be derived as a result of wastes recycling, etc. if the limestone used in the past can be substituted by application to the Flue Gas Desulfurization process of the limestone sludge as a byproduct of iron-making processes.

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